



Floodplain Technical Memorandum

ArDOT JOB NO. CA0602

I-30 (From I-530/I-440 to I-40) and
I-40 (From Hwy. 365/MacArthur Dr. to Hwy. 67)
Pulaski County, Arkansas
October 2017



U.S. Department
of Transportation
**Federal Highway
Administration**



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- Attachment C: Volume Calculations
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1.0 INTRODUCTION

Approved by Arkansas voters, the Arkansas Department of Transportation (ArDOT) is implementing an accelerated State Highway Construction and Improvement Program named the Connecting Arkansas Program (CAP).

A major component of the CAP is to implement a project to improve a portion of Interstate 30 (I-30) from Interstate 530 (I-530) and Interstate 440 (I-440) to Interstate 40 (I-40), including the Arkansas River Bridge, and a portion of I-40 from Highway (Hwy.) 365 (MacArthur Drive [Dr.]) to Hwy. 67. This project is CA0602: I-530 - Hwy. 67 (Widening & Reconst.) (I-30 & I-40), commonly known as the 30 Crossing project. **Figure 1** illustrates the proposed 7.3-mile project limits.

1.1 Existing Facility

I-30 is one of the critical links of the Central Arkansas Freeway System. It connects communities within the Central Arkansas Region and serves local, regional and national travelers with varied destinations and trip purposes.

The I-30 corridor generally consists of three main lanes in each direction with parallel one-way discontinuous frontage roads on each side of the interstate. In the northern portion of the project limits, the I-40 corridor consists of three to four main lanes in each direction with parallel one-way frontage roads on each side of the interstate between the I-30/I-40 interchange and North Hills Boulevard (Blvd.). Within the 7.3-mile corridor, four system interchanges are located:

- I-30 with I-530 and I-440
- I-30 with I-630
- I-30 with I-40
- I-40 with Highways 67/167

1.2 Proposed Alternatives

1.2.1 No-Action Alternative

The No-Action Alternative represents the case in which the proposed project is not constructed, but could include future projects identified through the long range planning process for maintaining a state of good repair as funding becomes available.

1.2.2 Action Alternatives

Two different main lane configurations are under consideration. Both would include the replacement of the Arkansas River Bridge.

- Eight-Lane General Purpose (GP) Alternative would provide four main lanes in each direction with no Collector Distributor (C/D) lanes.
- Six-Lane with C/D Lanes Alternative would reconstruct the existing six-lane (three in each direction) roadway while adding two decision lanes on each side that ultimately feed into a C/D system located at the Arkansas River Bridge.

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FIGURE 1: LOCATION MAP



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1 The current Hwy. 10 (Cantrell Rd.) interchange provides direct access to the downtown
2 business district of Little Rock. Its proximity to the Arkansas River Bridge and the I-30
3 interchange with I-630 creates a unique level of complexity. In order to balance various
4 project goals, two interchange concepts are being considered for replacement of this
5 interchange:

- 6 • An elevated Single Point Urban Interchange (SPUI) constructed in the same location
7 as the current interchange;
- 8 • A Split Diamond Interchange (SDI) constructed south of the existing interchange at
9 4th and 9th Streets.

10
11 Combining the two main lane configurations with the two Hwy. 10 (Cantrell Rd.) interchange
12 concepts results in the four Action Alternatives as follows:

- 13
14 Alternative 1A: 8-Lane GP with SPUI Alternative
- 15 Alternative 1B: 8-Lane GP with SDI Alternative
- 16 Alternative 2A: 6-Lane with C/D Lanes with SPUI Alternative
- 17 Alternative 2B: 6-Lane with C/D Lanes with SDI Alternative

18
19 For detailed information on the Action Alternatives, refer to the **30 Crossing**
20 **Environmental Assessment** (EA) for the proposed project.

21 22 2.0 REGULATORY BACKGROUND

23
24 The following regulatory requirements listed below apply to the floodplains located within
25 the 30 Crossing project area.

- 26
27 • **Executive Order (EO) 11988, Floodplain Management (1977)** directs federal
28 agencies to “provide leadership and take action to reduce the risk of flood loss, to
29 minimize the impacts of floods on human safety, health and welfare, and to restore
30 and preserve the natural and beneficial values served by floodplains.” This EO was
31 authorized to assist in furthering the National Environmental Policy Act (NEPA),
32 the National Flood Insurance Act of 1968 (amended), and the Flood Disaster
33 Protection Act of 1973.
- 34 • **23 Code of Federal Regulations (CFR), Part 650 – Highways, Chapter I –**
35 **Federal Highway Administration, U.S. Department of Transportation, Part**
36 **650 – Bridges, Structures, and Hydraulics**, prescribes the policies and
37 procedures that the FHWA is directed to implement in the “location and hydraulic
38 design of highway encroachments on floodplains.”
- 39 • **44 CFR Part 1 – Emergency Management and Assistance, Chapter I – FEMA,**
40 contains the basic policies and procedures of the Federal Emergency
41 Management Agency (FEMA) to regulate floodplain management and to analyze,
42 identify, and map floodplains for flood insurance purposes.

3.0 METHODOLOGY

Floodplains are the areas that are inundated during a storm of given magnitude. A 100-year floodplain is the regulatory floodplain associated with a 100-year design storm frequency, or base flood. Floodplains are designated on mapping used by the FEMA flood insurance program. The floodplain associated with the base flood is designated Zone A, AE, or AH. The FEMA designated flood zones are shown on the FEMA Floodplain maps in **Attachment A** for the project area. The project area intersects the 100-year floodplain at Fourche Creek, Arkansas River, and the Dark Hollow Basin.

Changes in the floodplain, such as adding fill material, constructing buildings or bridges, or constricting the channel, can cause a rise in the water surface elevation. This increase in the water surface elevation can subsequently impact properties not previously affected and are consequently regulated by FEMA. Floodplain impacts are measured by the change in the water surface elevation or Base Flood Elevation (BFE).

The floodway is a portion of the floodplain and stream channel reserved for the passage of flood waters while providing for suitable use of the adjacent land. It must be kept free of encroachment in order to carry the base flood without increasing the water surface more than a designated height. Hydraulic modeling is used to generate the floodway limits, which are site specific to each stream channel. Delineating a floodway requires an analysis of the effects of eliminating areas of flow in the overbanks on computed water surface elevations. Within the project area, the Arkansas River and Fourche Creek have designated floodways.

Detailed HEC-RAS flood models have been developed for Fourche Creek and for the Arkansas River. Flood elevations in those locations are therefore listed at Zone AE, meaning BFE's are determined. The Arkansas River HEC-RAS model was modified to include the proposed I-30 bridge. This evaluation is presented in a separate report, the I-30 Arkansas River Bridge Replacement Bridge Hydraulics Report.

The Fourche Creek floodway is considered Zone AE, meaning that BFE's have been determined by hydraulic modeling. The analysis presented herein for Fourche Creek is volumetric only. Fill volumes were calculated between the ground surface elevation, and the BFE at the locations of encroachment (elevation 256.5 NAVD).

Dark Hollow is considered Zone AH, meaning BFE's were developed to reflect 1-3 feet of ponding. Surveys performed for this project allowed the exact limits of the 100-year floodplain to be determined and represented as the 252-foot contour for the purposes of estimating fill and compensation volumes. Fill and compensation volume calculations were performed using these floodplain limits rather than the estimated limits shown on the Flood Insurance Rate Maps (FIRM), included as **Attachment A**. The analysis presented herein for Dark Hollow is volumetric only. For both Action Alternatives, permanent fill volumes were calculated between the ground surface elevation, and the BFE for Dark Hollow (252). Any permanent excavation occurring as a result of the project between those elevations was deducted from the fill volume.

1 The vertical datum used to identify elevations in this memo is North American Vertical
2 Datum (NAVD) 1988. The horizontal datum used to identify the location of the project
3 and floodplains is North American Datum (NAD) 83, GRS80 spheroid.

4 5 4.0 EXISTING CONDITIONS 6

7 Fourche Creek begins at the foot of Brush Mountain, near Ferndale, approximately
8 20 miles northwest of the southern end of the proposed project. Fourche Creek flows
9 southeast through the southern end of the project area to join with the Arkansas River,
10 5 miles southeast of the project area. The FEMA designated floodway of Fourche Creek
11 passes through the I-30, I-530, and I-440 interchange (**Figure 1**). The channel of Fourche
12 Creek meanders through the interchange, crossing I-440 at several locations.

13
14 The Dark Hollow Basin, a ponding/flood detention area, is located along the I-40 corridor
15 in the northern portion of the project area, from the I-30/I-40 interchange to the I-40/US
16 67 interchange (**Figure 2**). There is no FEMA designated floodway for the Dark Hollow
17 Basin. The Dark Hollow Basin is drained by two major drainage channels, referred to in
18 the *North Little Rock, Dark Hollow Limited Re-Evaluation Report (USACE, 2002)* as the
19 Pike Diversion Ditch (PD1) and Dark Hollow Channel (DH 2/3). Pike Diversion Ditch
20 originates near the I-30/I-40 interchange, where it is identified on FIRM Map
21 05119C0344G as Fairman Ditch Tributary 1. Downstream of I-30, PD1, which is shown
22 on USGS Quad maps as the Fairman Ditch, continues east for approximately 4700 feet
23 before turning south. Dark Hollow Channel (DH3) originates on the east side of the North
24 Hills interchange, passes under I-40, and drains south and east under the Union Pacific
25 Railroad (UPRR). Dark Hollow Channel is shown on USGS Quad maps as Ditch Six.
26 South of the UPRR crossing, Dark Hollow Channel joins with a channel originating to the
27 east called Dixie Addition (DA). South of the point of confluence of DH3 and DA, Dark
28 Hollow Channel is designated DH2. PD1 drains through the Dark Hollow Basin, passing
29 under the UPRR, and unites near Sam Evans Drive with DH2, forming DH3, which
30 continues along Range Line Avenue for about 1500 feet. At this point the channel enters
31 the Redwood Tunnel, an arch-shaped culvert running underground along North Redwood
32 Street for approximately 2,700 feet, where it discharges into the Arkansas River. The
33 Redwood Tunnel was identified in the *North Little Rock, Dark Hollow Limited
34 Re-Evaluation Report (USACE, 2012)* as undersized with respect to the flow it carries.

35
36 In an effort to evaluate alternatives to alleviate flooding in the Dark Hollow Basin, the
37 *North Little Rock, Dark Hollow Limited Re-Evaluation Report (USACE, 2012)* analyzed
38 conveyance and storage improvements using HEC-HMS and HEC-RAS. The *North Little
39 Rock Dark Hollow Limited Re-Evaluation Report (USACE, 2011)* recommended
40 conveyance improvements focused on the existing channels and the Redwood Tunnel,
41 as well as storage improvements located in the Dark Hollow floodplain.

42
43 The existing conditions water surface elevations from the hydraulic model in the *North
44 Little Rock, Dark Hollow Limited Re-Evaluation Report (USACE, 2012)* agrees with the
45 BFE of 252 shown on the FIRM maps for the Dark Hollow Basin. The elevation 252
46 contour was therefore considered to be the limit of the base flood for the purpose of
47 calculating potential floodplain impacts from the project in the Dark Hollow Basin.
48

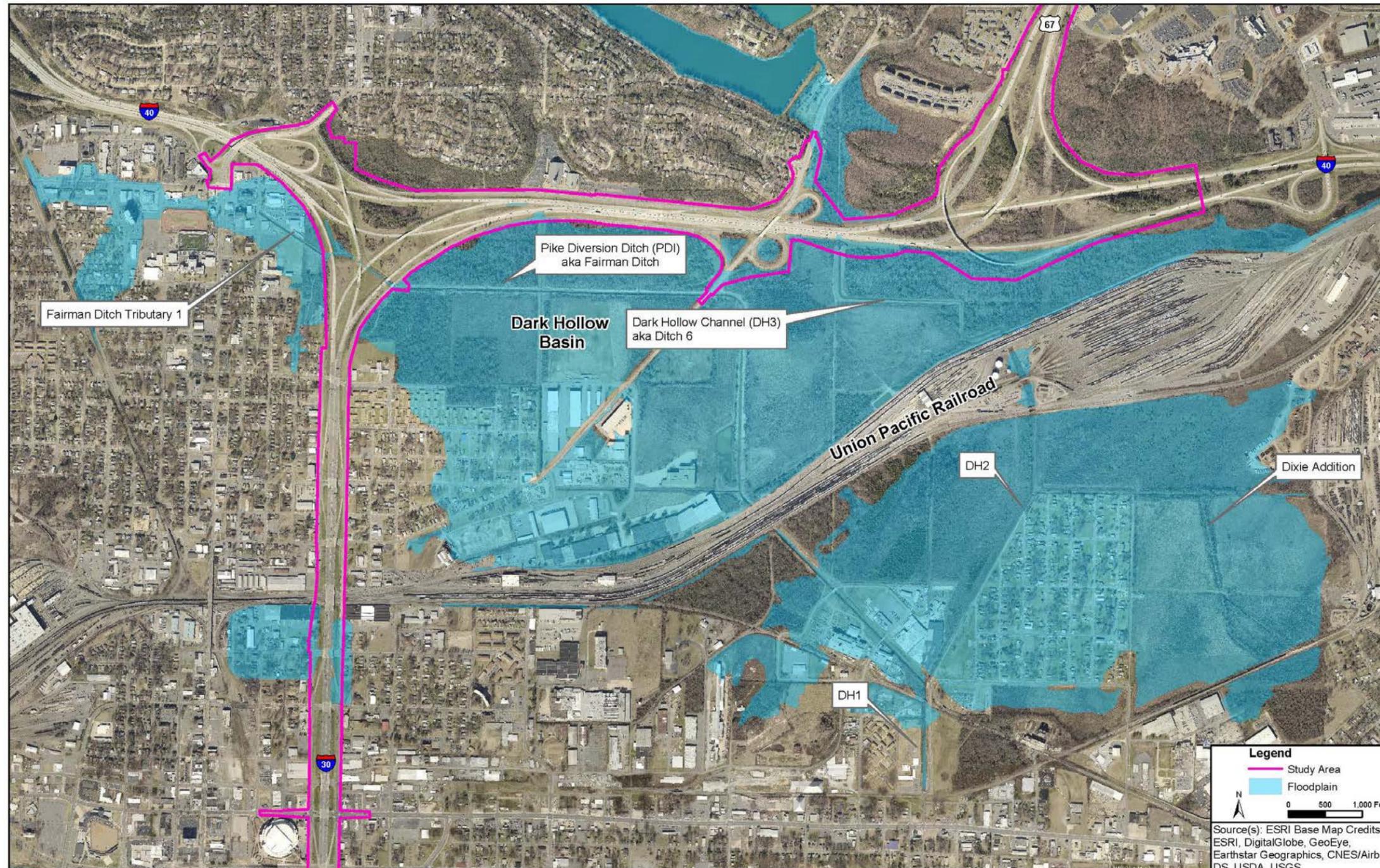
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FIGURE 2: DARK HOLLOW FLOODPLAIN



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2 5.0 IMPACTS AND MITIGATION
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4 5.1 No-Action Alternative
5

6 The No-Action Alternative would have no effect on floodplains.
7

8 5.2 Proposed Action Alternatives
9

10 The proposed Action Alternatives would raise and widen I-30, which has the
11 potential for placing fill in floodplains at Fourche Creek and Dark Hollow. The
12 estimated impacts from the Action Alternatives on floodplains are given in Sections
13 6.2.1 and 6.2.2.

14 5.2.1 Fourche Creek
15

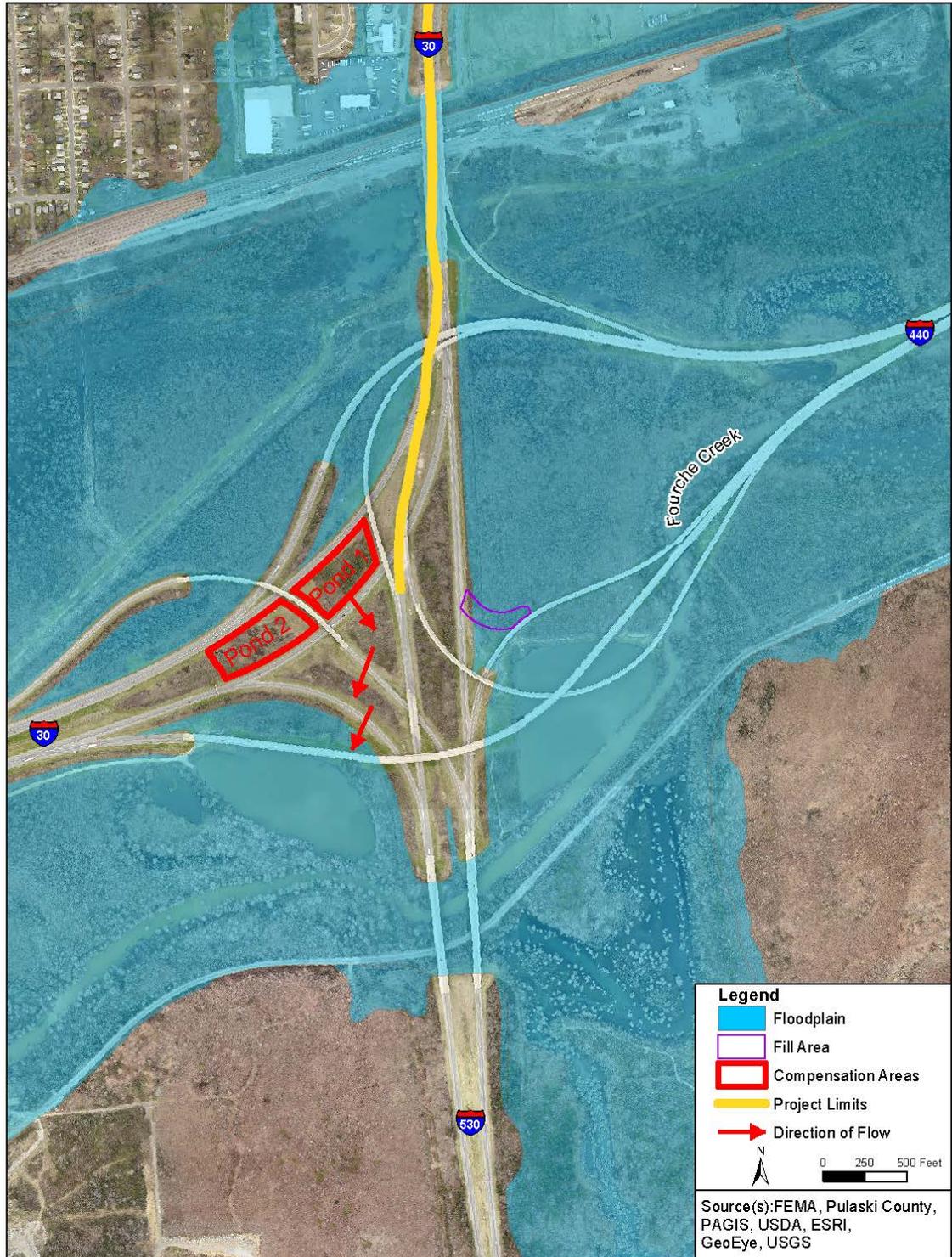
16 The conceptual maintenance of traffic plan developed for this project requires that
17 fill would have to be temporarily placed within the floodway associated with Fourche
18 Creek to construct a temporary ramp from I-440 westbound to I-30 northbound. The
19 fill would be located north of the channel of Fourche Creek, immediately on the
20 downstream (east) side of I-530. Consequently, while this area provides storage of
21 flood waters, it is in an ineffective flow area. The temporary fill would be removed
22 following construction, but volume compensation is being proposed to account for
23 the possibility of a flooding event occurring during construction. For both the 8-Lane
24 G P and 6-Lane with C/D Alternatives, the temporary fill volume is approximately
25 11.2 Acre-feet (Ac-ft), calculated between the existing ground surface and the BFE
26 of 256.5 (**Figure 3**). In addition to this temporary fill, the proposed bridge over the
27 Fourche Creek floodplains would be wider than the existing bridge, resulting in
28 approximately 0.1 Ac-ft of additional permanent fill due to bridge piers.
29

30 The proposed compensating areas (Ponds 1 and 2) are located west of I-530, in the
31 median of I-30. Ponds 1 and 2 would be connected, under the elevated I-530
32 northbound to I-30 westbound ramp, during flood events. The compensation areas
33 would be connected to Fourche Creek under I-30 to the south so that they would fill
34 as flood waters rise in Fourche Creek. The exact method of making this connection
35 would be the responsibility of the Design Builder. The proposed compensating
36 volume is 11.93 Ac-ft. This compensation addresses an anticipated temporary
37 condition; however, the compensation is permanent and can be used to offset other
38 floodplain impacts in Fourche Creek with either this or other projects.
39

40 The floodplain impacts to Fourche Creek and the conceptual mitigation plan were
41 discussed with the City of Little Rock at a meeting on January 11, 2017
42 (**Attachment D**). The City of Little Rock requested that the Design Builder provide
43 a “no-rise” certification for the Fourche Creek crossing and approved the conceptual
44 mitigation plan.
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FIGURE 3: TEMPORARY FLOODPLAIN FILL AND COMPENSATING STORAGE AREAS IN I-30/I-530/I-440 INTERCHANGE



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1 5.2.2 Dark Hollow
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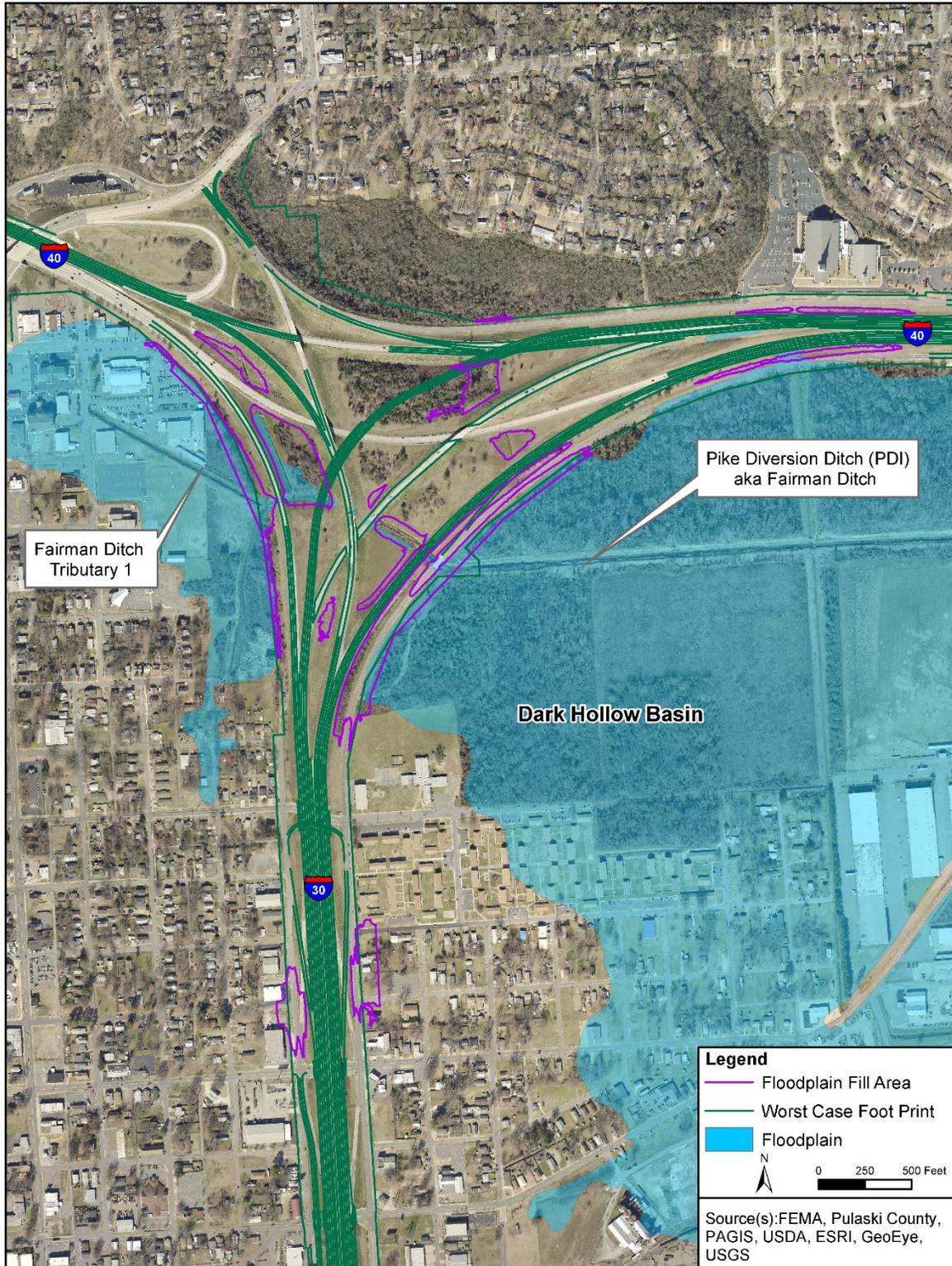
3 It is not possible to widen the roadway and avoid placing additional fill in the Dark
4 Hollow floodplain. Encroachment is minimized with both Action Alternatives by
5 bridging the floodplains wherever feasible.
6

7 In Dark Hollow, approximately 18.01 Ac-ft of permanent fill would be placed below
8 elevation 252 with the 8-Lane GP Alternative, and 17.43 Ac-ft of permanent fill would
9 result from the 6-lane with C/D Alternative (**Figures 4 and 5**).
10

11 Mitigation in the form of compensatory storage would be created to replace the
12 storage lost in the Dark Hollow floodplain due to permanent roadway fill. In the I-30/I-
13 40 interchange, three areas were identified as contiguous and hydraulically
14 connected to the Fairman Ditch, which passes through the interchange from west to
15 east. These flood storage areas are shown on **Figure 6**. As flood surface elevations
16 rise in Fairman Ditch, flood waters would spill out of the channel and fill the
17 contiguous flood storage areas. The areas would be graded to allow flood waters to
18 drain to the Fairman Ditch (**Attachment B**). The exact method of making this
19 connection would be the responsibility of the Design Builder. The volume able to be
20 created in these three areas is 11.57 Ac-ft, 3.67 Ac-ft, and 10.85 Ac-ft, for a total of
21 26.09 Ac-ft. This is an excess of 8.08 Ac-ft over the worst case amount of fill that
22 would result from any of the Action Alternatives in the Dark Hollow floodplain.

23 The floodplain impacts to Dark Hollow and the conceptual mitigation plan were
24 discussed with the City of North Little Rock at a meeting on October 11, 2016
25 (**Attachment D**). The City of North Little Rock approved the conceptual mitigation
26 plan.

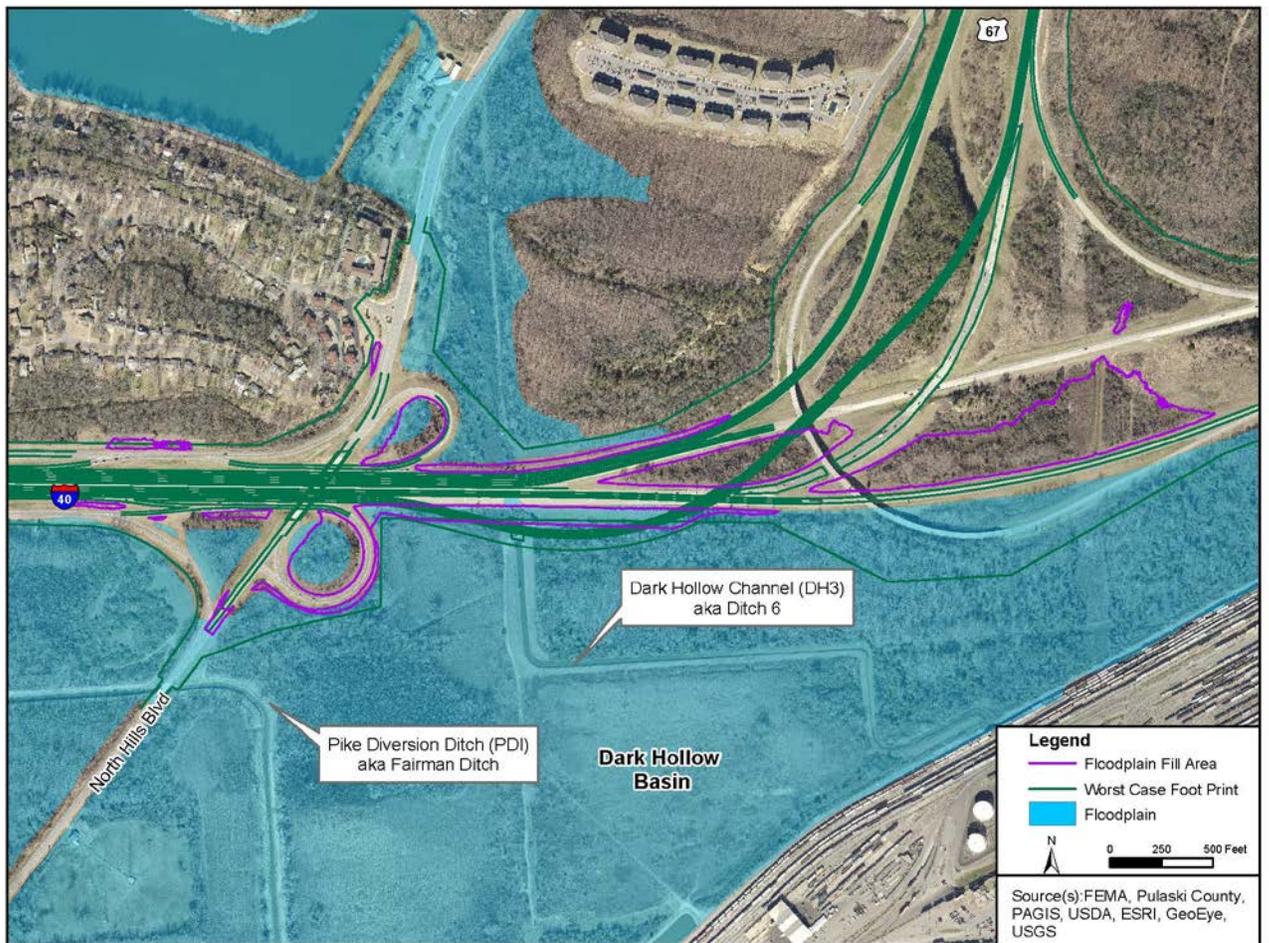
1 **FIGURE 4: PERMANENT FLOODPLAIN FILL AREAS IN DARK HOLLOW (I-30/I-40 INTERCHANGE)**



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**FIGURE 5: PERMANENT FLOODPLAIN FILL AREAS IN DARK HOLLOW AREA
(NORTH HILLS INTERCHANGE)**

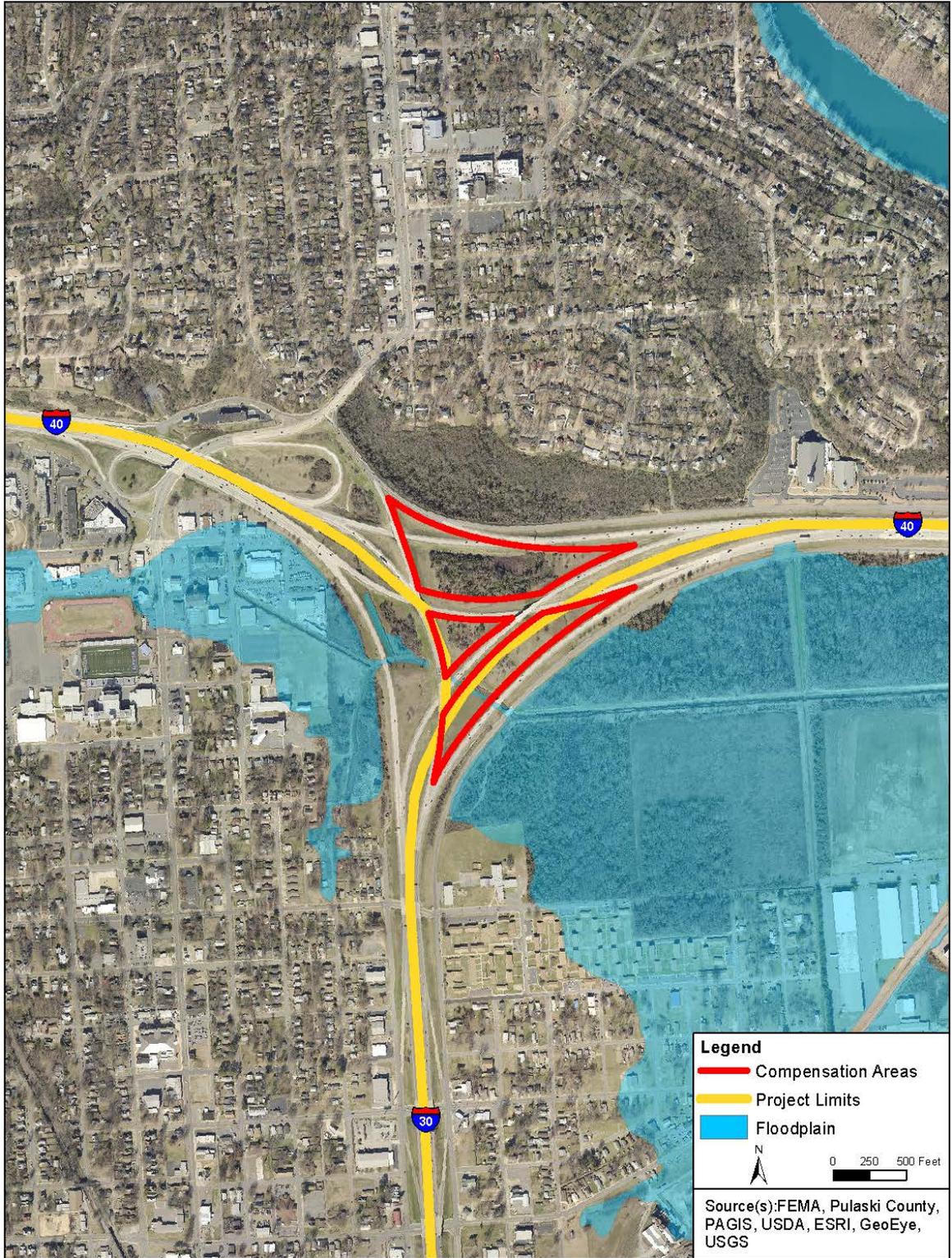


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FIGURE 6: FLOODPLAIN COMPENSATION AREAS FOR DARK HOLLOW BASIN



3

1 6.0 SUMMARY AND CONCLUSIONS

2

3 The proposed 30 Crossing Action Alternatives are expected to involve encroachment into
4 the 100-year floodplains of Fourche Creek, the Arkansas River, and Dark Hollow. These
5 encroachments are unavoidable and, as a result of minimization and mitigation measures,
6 would not result in an increase in floodplain elevations or loss of floodplain storage.

7 7.0 REFERENCES

8

9 Federal Emergency Management Agency (FEMA). Flood Insurance Study Pulaski
10 County, Arkansas, and Incorporated Areas Volume 1 of 3. July 2015.

11

12 Federal Emergency Management Agency (FEMA). Flood Insurance Study Pulaski
13 County, Arkansas, and Incorporated Areas Volume 2 of 3. July 2015.

14

15 U.S. Army Corps of Engineers. North Little Rock, Dark Hollow Limited Re-Evaluation
16 Report. Appendix A: Hydrology and Hydraulics Report. April 2002 (Updated April 2006).

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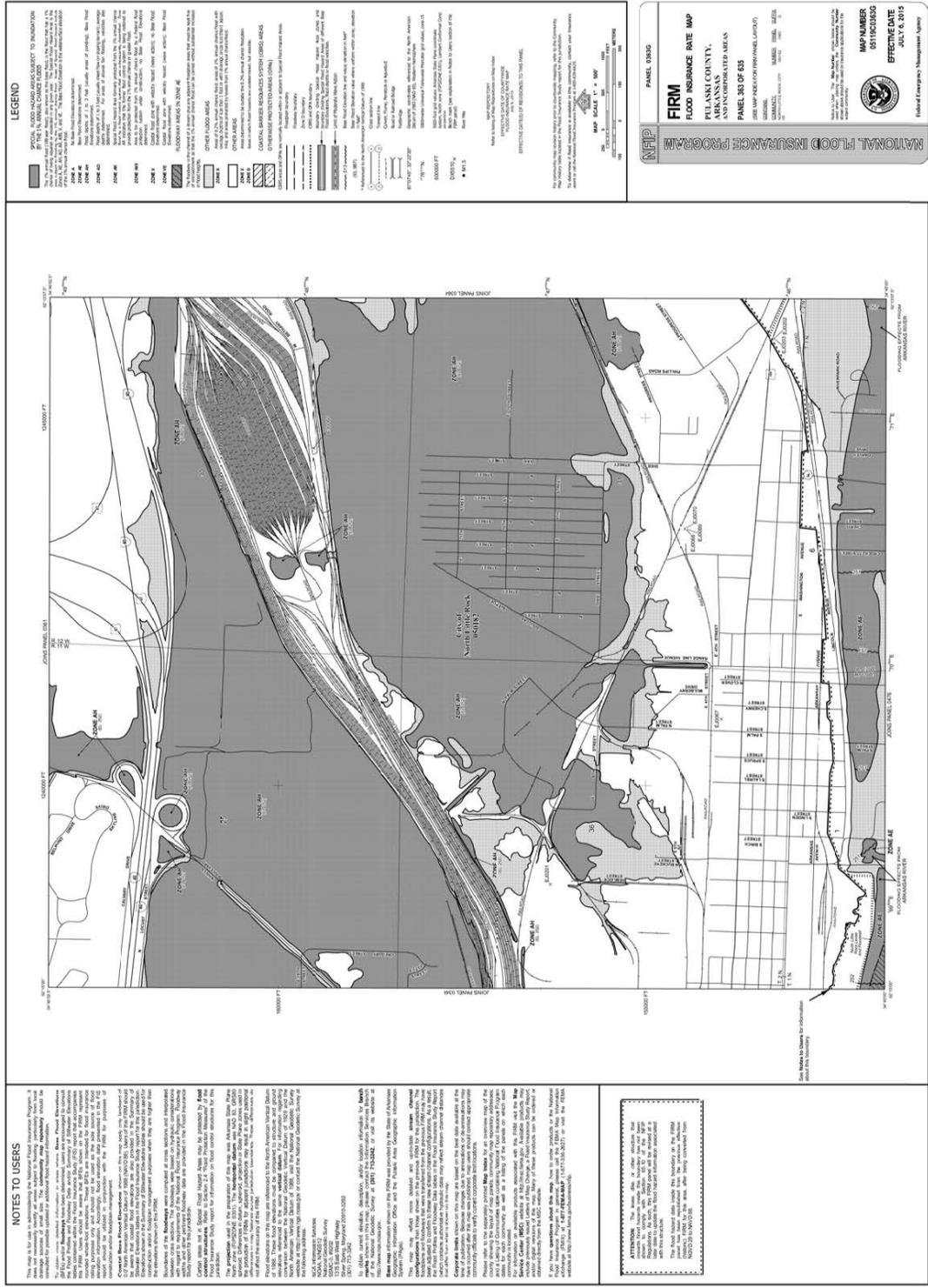
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Attachment A: Flood Insurance Rate Maps

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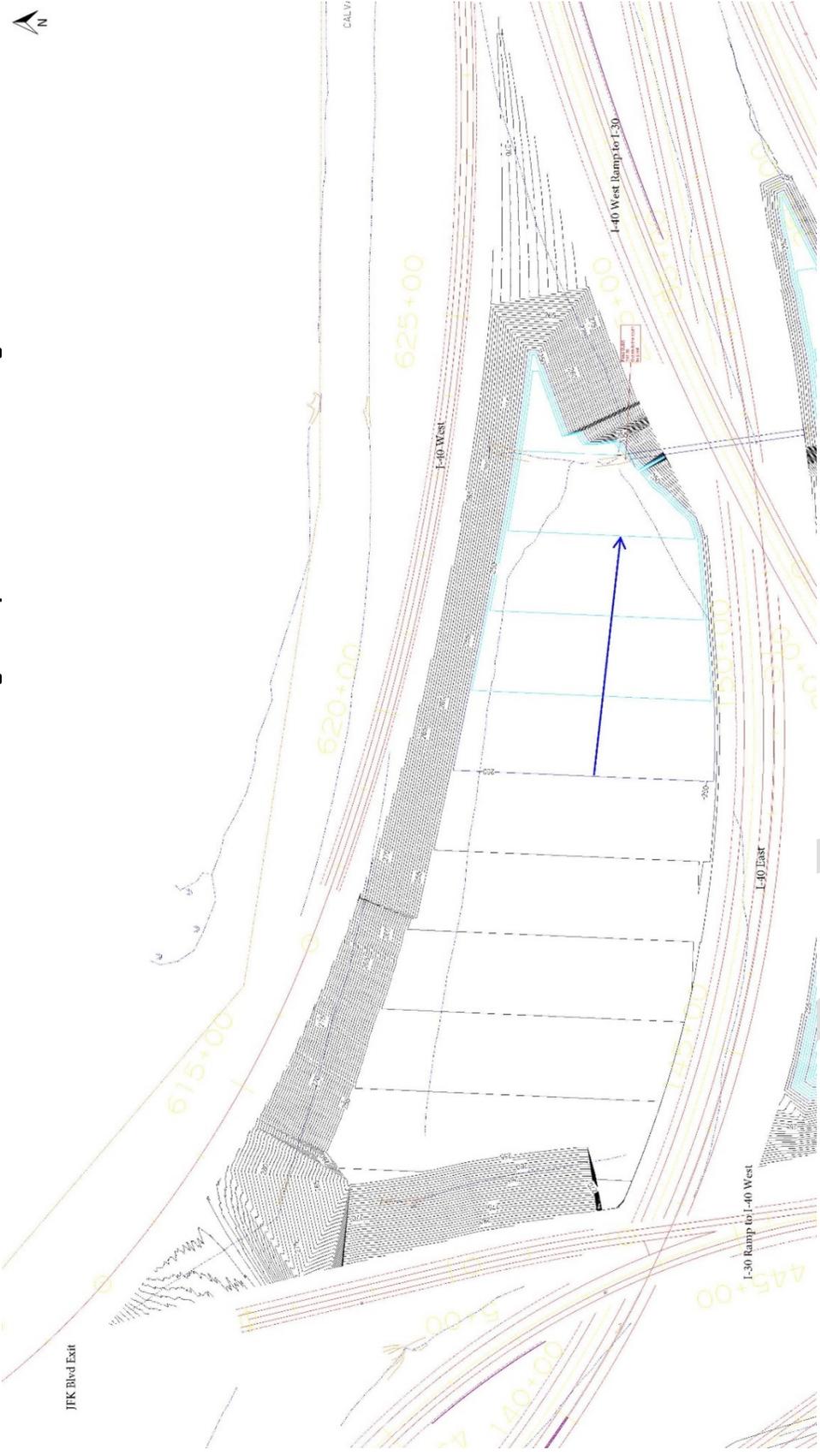
Attachment A-4 Firm Map 363



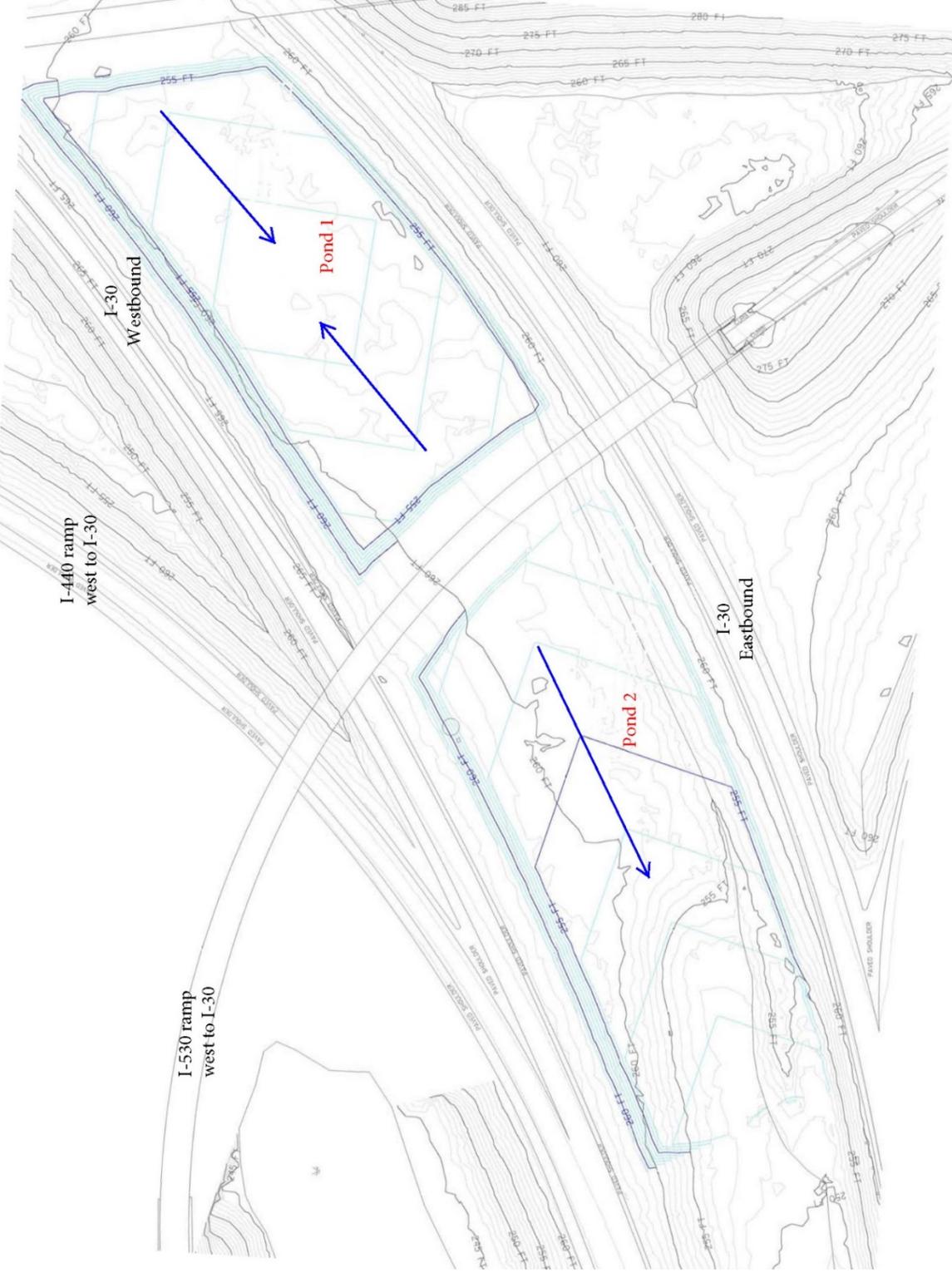
Attachment B: Grading Plan for Floodplain Compensation Areas

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Attachment B-2 North Interchange Compensation Area Grading



Attachment B-3 South Interchange Compensation Area Grading



Attachment C: Volume Calculations

Revised Floodplain Compensating Storage Volumes at Southern Terminus of Project due to Temporary Detour for Reconstruction of I-440 WB to I-30 EB Ramp

PREPARED FOR: AHTD
COPY TO: GarverUSA
PREPARED BY: CH2M --Tim Walsh *TBW*
DATE: August 12, 2016
PROJECT NUMBER: 657528

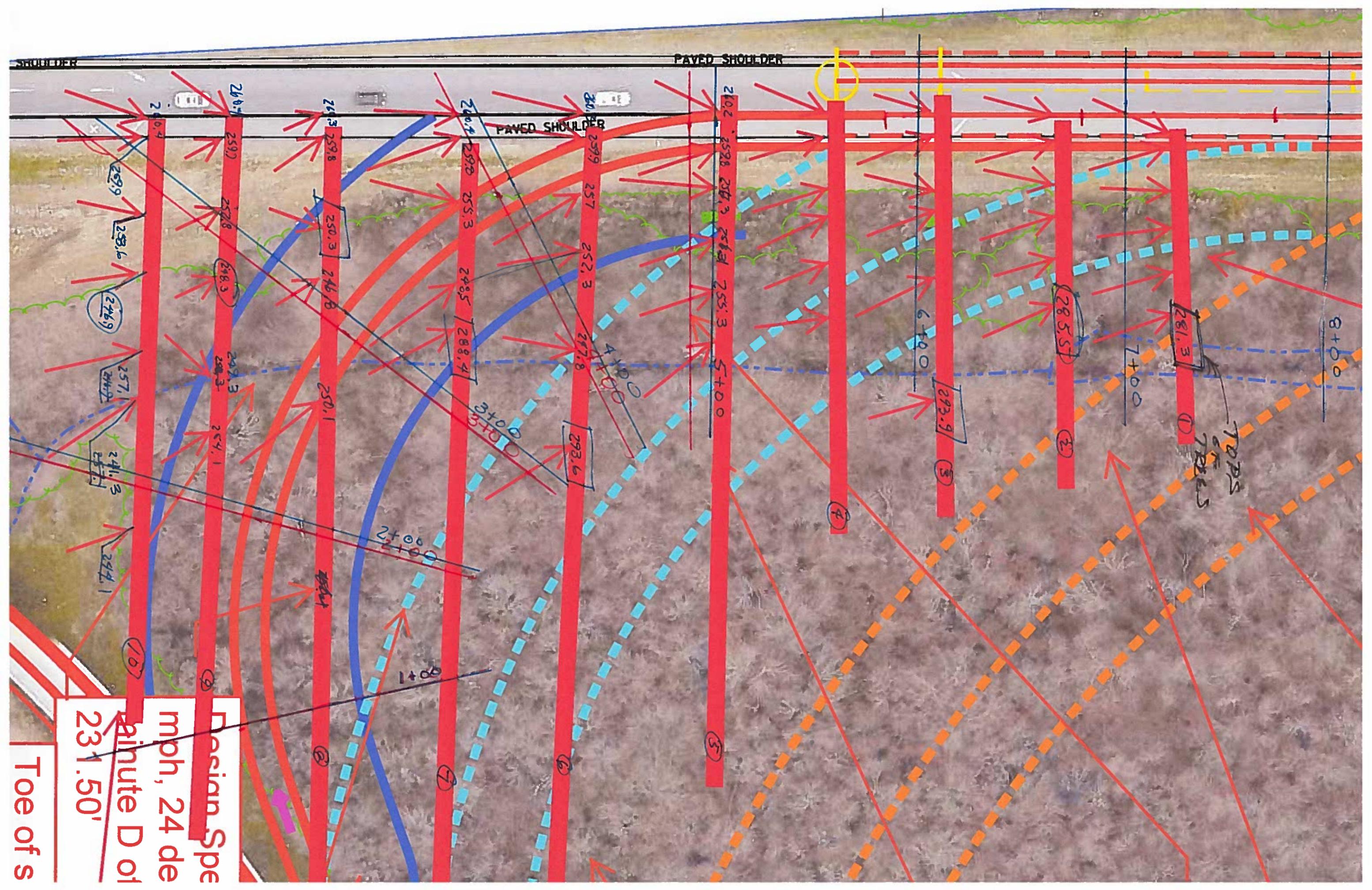
APPROVED BY: CH2M--Mark Callahan *MSC*

In order to reconstruct portions of the I-440 WB to I-30 EB ramp but maintain this movement, a temporary detour is necessary. This detour is to be constructed by partially widening certain causeway bridge structures plus constructing an earthen berm portion. Previously, an estimate of the fill volumes between normal ground and the floodplain elevation of 256.5 were prepared. However, that estimate was based upon an assumption that the natural ground elevation was at elevation 236. This assumed elevation was based upon limited survey information. Google Earth files were utilized to obtain natural ground elevation estimates. However, it was apparent that the elevations within the treelines were the actual tops of trees and not representative of the actual ground. The assumed existing ground elevation at the creek (236) was obtained from an unobscured area. It was recognized that the resulting compensating storage volume estimate based upon the natural ground elevation of 236 was very conservative.

Mr. John Cantabery (Garver) suggested that utilizing county LIDAR data through PAGIS may give more realistic elevations. A revised estimate of the required compensating storage volume was prepared using this LIDAR information.

This revised estimate was based upon preparing cross sections at 100 foot intervals along the proposed detour alignment and calculating volumes by average end area method. Worksheets and calculations are attached.

Based upon this revised and more detailed engineering analysis, it was computed that the compensating storage volume for the earthen embankment of this temporary detour ramp is 18,069 cys or 11.2 acre-feet.



PAVED SHOULDER

PAVED SHOULDER

TOPS OF TREES

Design Speed
 24 mph
 Design Life
 20 years
 Design Flood
 100 year
 Toe of slope
 231.50'

260.4

259.2

261.3

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 The points below match up with the arrows. Work your way
 from left to right.

LINE	EOL	EOS	E/W	MID	TOE	WOODS
1	260.5	260.1	252.2	251	249.7	281.3

LINE	EOL	EOS	E/W	MID	TOE	WOODS
2	260.4	260	256.8	252.5	247.1	285.5

LINE	EOL	EOS	E/W	MID	TOE	WOODS
3	260.4	259.9	254.2	250.6	247.9	293.9

LINE	EOL	EOS	E/W	MID	TOE	WOODS
4	260.4	259.9	256	255.6	252.2	289.7

LINE	EOL	EOS	E/W	MID	TOE	WOODS
5	260.2	259.8	256.3	256.1	255.3	293.1

LINE	EOL	EOS	E/W	MID	TOE	WOODS
6	260.3	259.9	257	252.3	247.8	293.6

LINE	EOL	EOS	MID	E/W	TOE	WOODS
7	260.4	259.8	255.3	1	248.5	288.4

LINE	EOL	EOS	MID	E/W	TOE	WOODS
8	260.3	259.8	250.3	1	246.8	250.1

LINE	EOL	EOS	MID	TOE	E/W	STREAM	WOODS
9	260.4	259.9	252.8	248.3	1	249.3	254.1

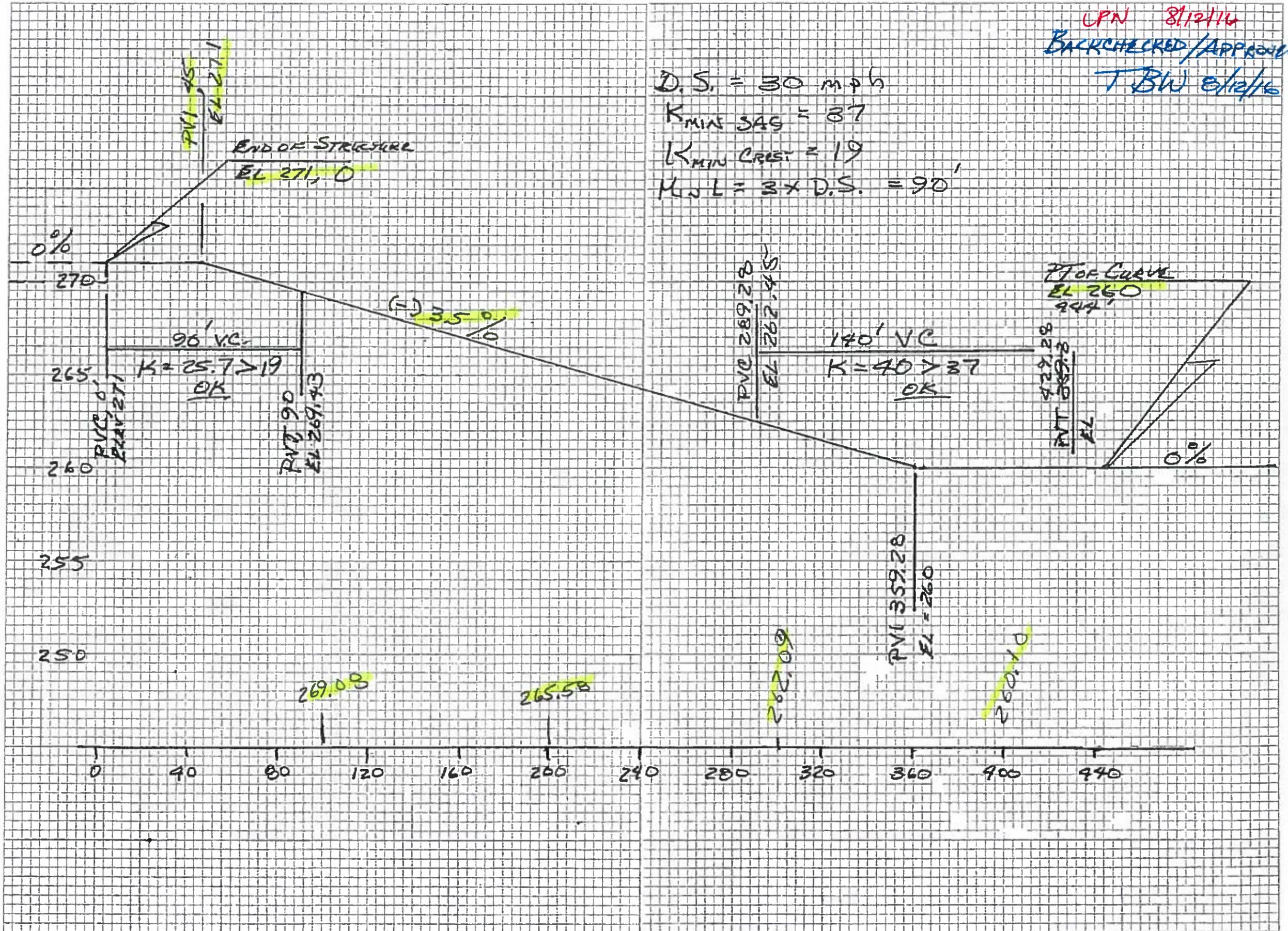
LINE	EOL	EOS	MID	TOE	E/W	WOODS	STREAM	WOODS
10	260.4	259.9	253.6	246.9	1	257.1	241.3	244.1

POINTS REPRESENT

EOL Edge of Lane
 EOS Edge of Shoulder
 MID Mid Point of Slope
 TOE Toe of Slope
 E/W Edge of Woods
 WOODS In Woods

NOTES:

1 Same point as point to the left. For example in line 7, one arrow represents the MID point and E/W point with an elevation of 255.3



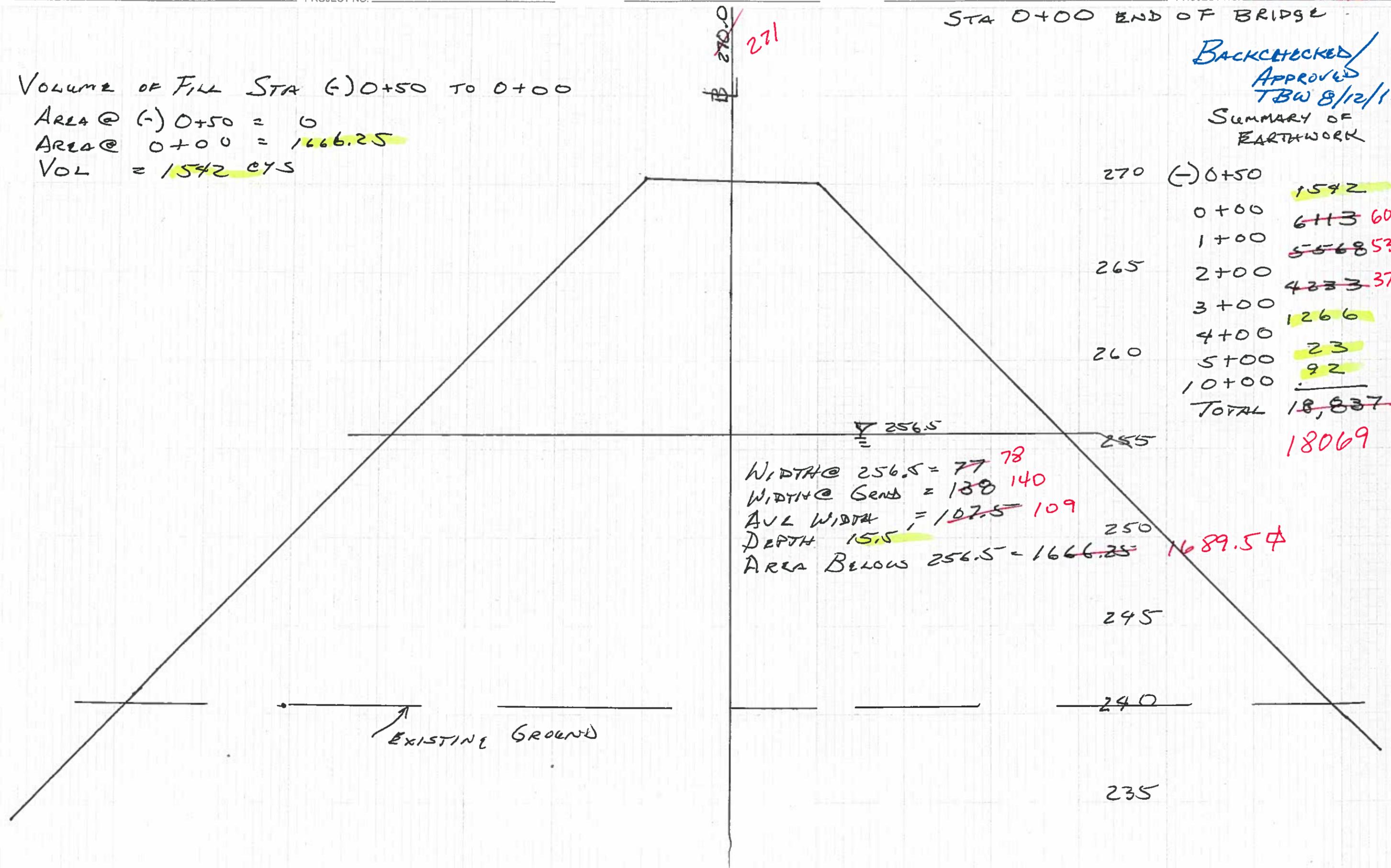
D.S. = 30 mph
 $K_{MIN} SAG = 37$
 $K_{MIN} CREST = 19$
 $MIN L = 3 \times D.S. = 90'$

UPN 8/12/16
 BACKCHECKED/APPROVED
 T BW 8/12/16

STA 0+00 END OF BRIDGE

BACKCHECKED/
APPROVED
TBW 8/12/16
 SUMMARY OF
 EARTHWORK

VOLUME OF FILL STA (-) 0+50 TO 0+00
 AREA @ (-) 0+50 = 0
 AREA @ 0+00 = 1666.25
 VOL = 1542 CYS



270	(-) 0+50	<u>1542</u>
	0+00	6113 6026
	1+00	5568 5396
265	2+00	4233 3724
	3+00	<u>1266</u>
	4+00	<u>23</u>
260	5+00	<u>92</u>
	10+00	<u> </u>
	TOTAL	18,837 <u>18069</u>

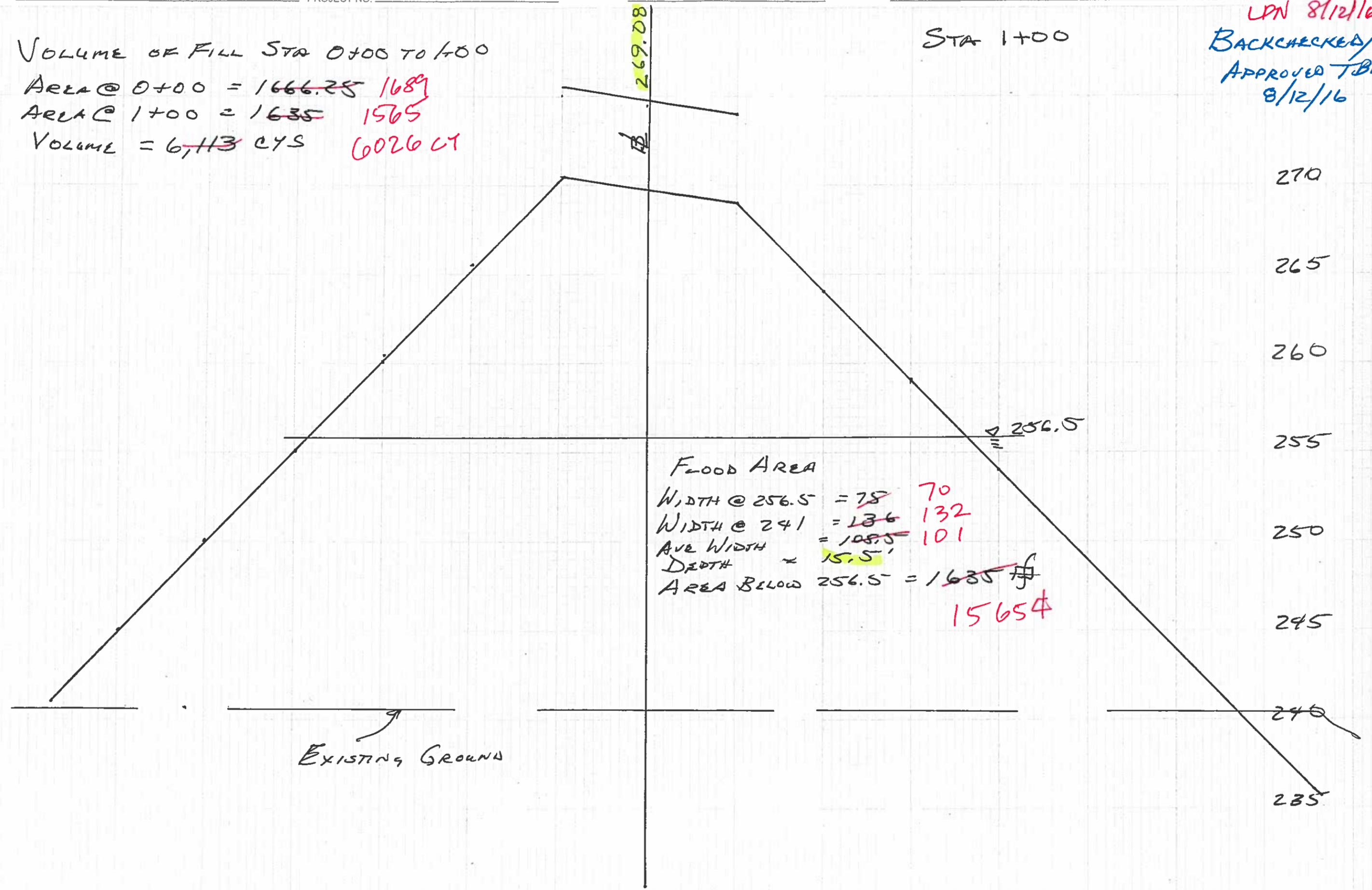
WIDTH @ 256.5 = ~~77~~ 78
 WIDTH @ GEND = ~~138~~ 140
 AVE WIDTH = ~~107.5~~ 109
 DEPTH 15.5
 AREA BELOW 256.5 = ~~1666.25~~ 1689.5 ϕ

EXISTING GROUND

VOLUME OF FILL STA 0+00 TO 1+00
 AREA @ 0+00 = ~~1666.25~~ 1689
 AREA @ 1+00 = ~~1635~~ 1565
 VOLUME = ~~6,113~~ CYS 6026 CY

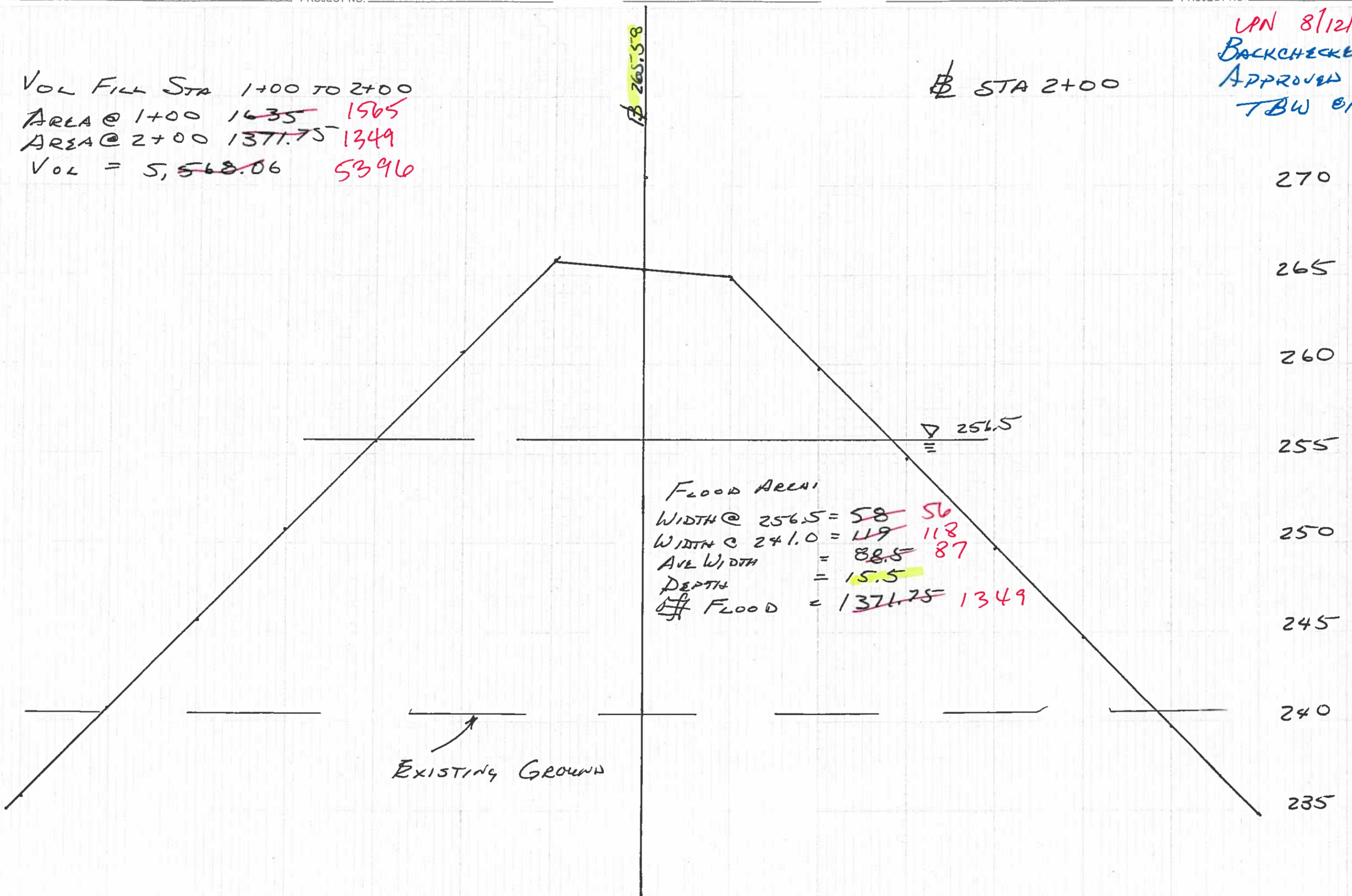
STA 1+00

LPN 8/12/16
 BACKCHECKED/
 APPROVED TBW
 8/12/16



VOL FILL STA 1+00 TO 2+00
 AREA @ 1+00 ~~1635~~ 1965
 AREA @ 2+00 ~~1371.75~~ 1349
 VOL = ~~5,568.06~~ 5396

UPN 8/12/16
 BACKCHECKED/
 APPROVED
 TBW 8/12/16

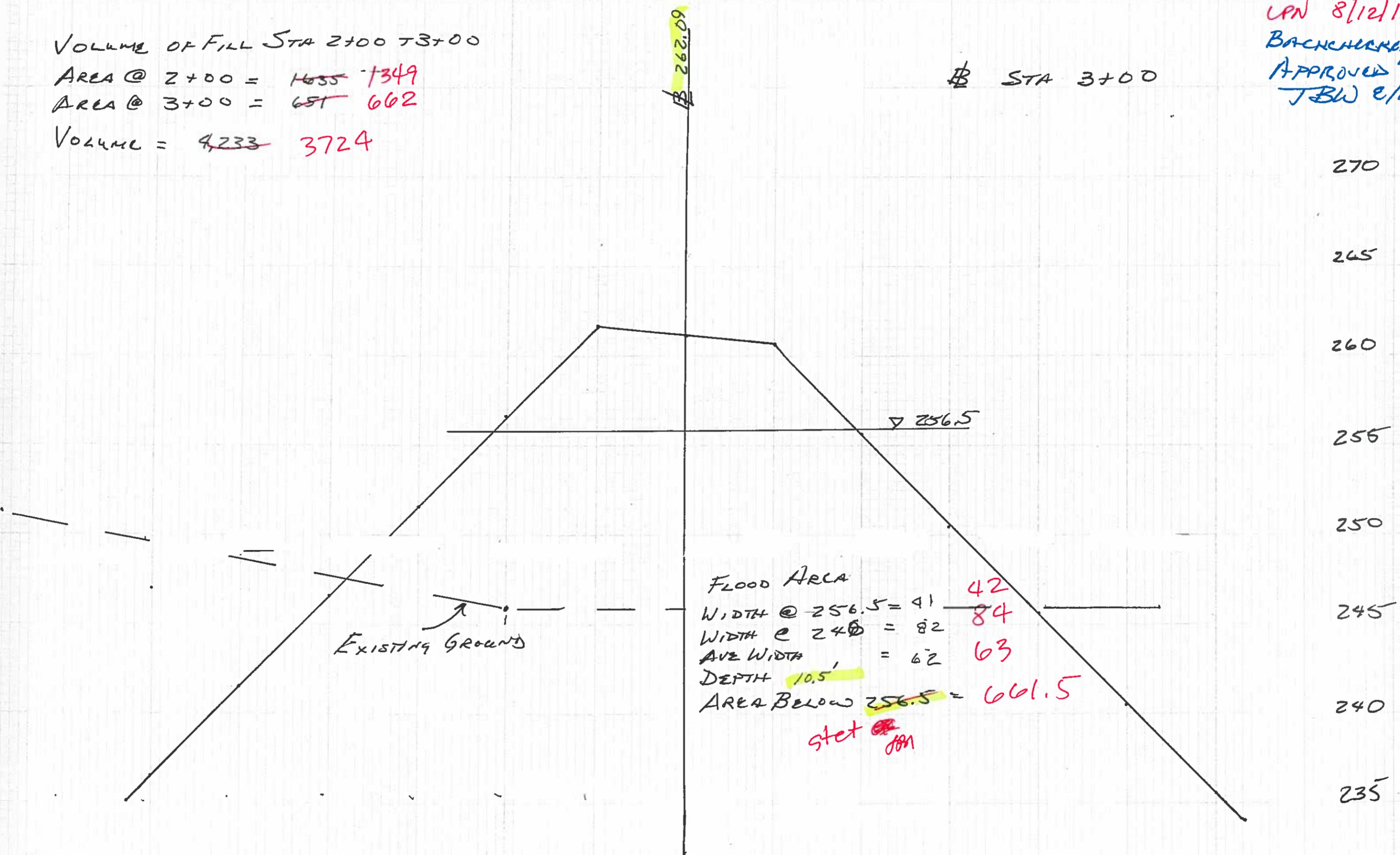


FLOOD AREA
 WIDTH @ 256.5 = ~~58~~ 56
 WIDTH @ 241.0 = ~~119~~ 118
 AVE WIDTH = 88.5 87
 DEPTH = 15.5
 FLOOD = ~~1371.75~~ 1349

270
 265
 260
 255
 250
 245
 240
 235

VOLUME OF FILL STA 2+00 TO 3+00
 AREA @ 2+00 = ~~1655~~ 1349
 AREA @ 3+00 = ~~651~~ 662
 VOLUME = ~~4,233~~ 3724

UPN 8/12/16
 BACKCHECKED/
 APPROVED
 TBW 8/12/16



FLOOD AREA
 WIDTH @ 256.5 = 41 42
 WIDTH @ 240 = 82 84
 AVE WIDTH = 62 63
 DEPTH 10.5'
 AREA BELOW 256.5 = 661.5
 stet JAN

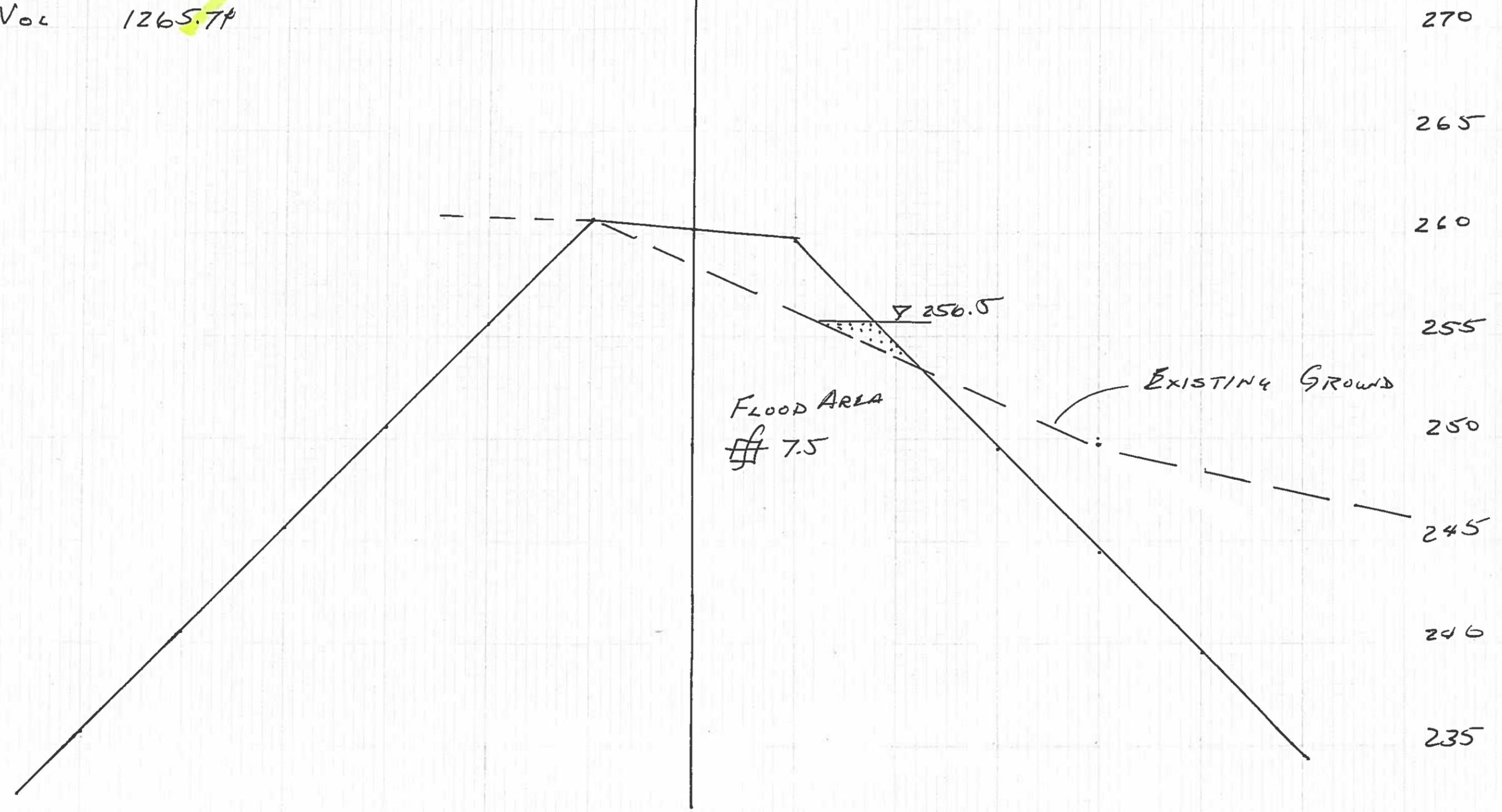
270
 265
 260
 255
 250
 245
 240
 235

VOLUME FROM 3+00 TO 4+00
 AREA @ 3+00 676
 AREA @ 4+00 7.5
 Vol 1265.74

LPN 8/12/16
 BACKCHECKED/
 APPROVED
 TBW 8/12/16

⊕ STA 4+00

01.092
 ⊕



FLOOD AREA
 ⊕ 7.5

EXISTING GROUND

270
 265
 260
 255
 250
 245
 240
 235

Volume 4+00 to 5+00

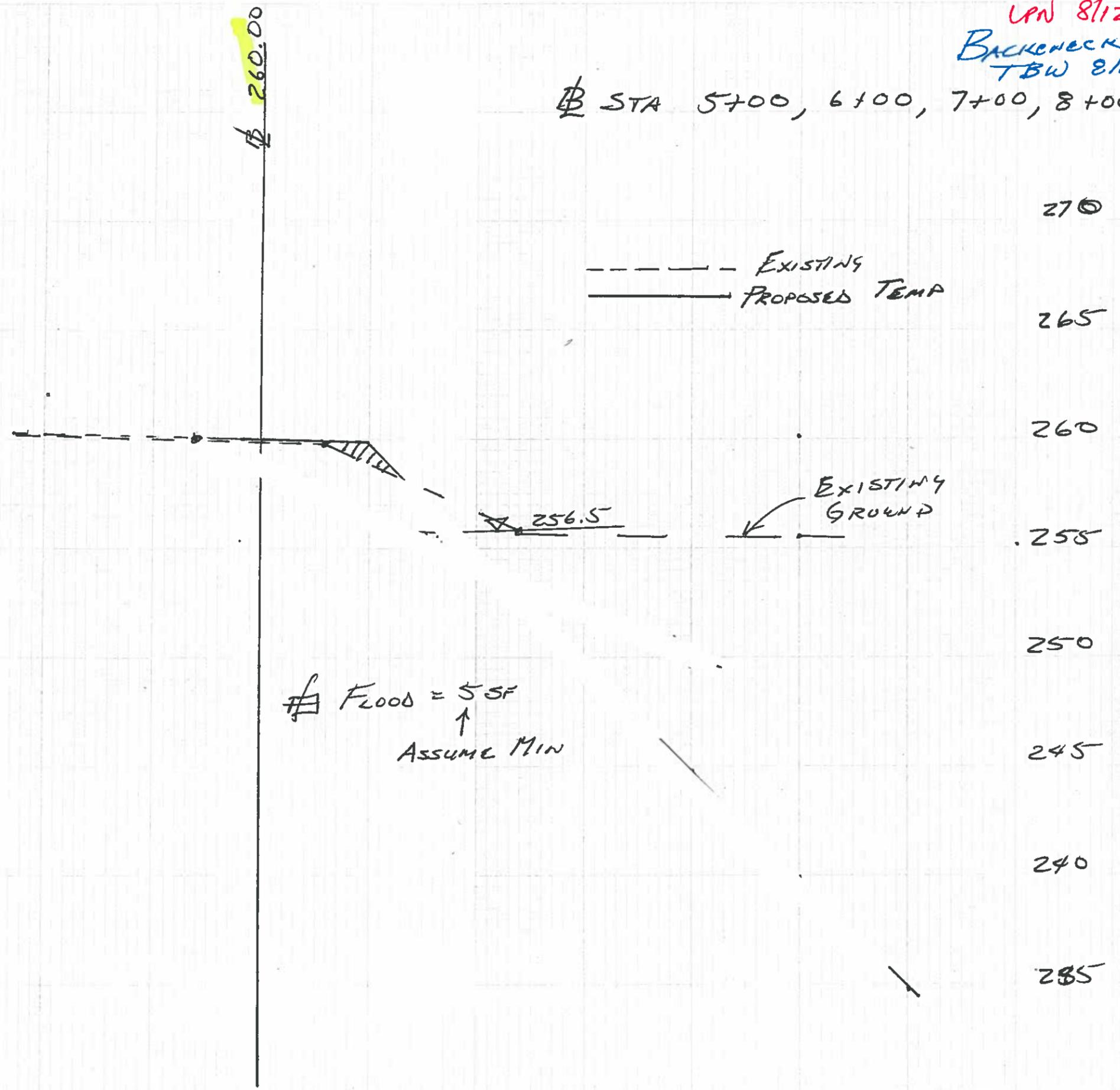
VOL 23 CYS

VOL 5+00 to 1.0+00

VOL 92 CYS

UPN 8/12/16
 BACKCHECKED/APP
 TBW 8/12/16

STA 5+00, 6+00, 7+00, 8+00, 9+00



Triangle Volume Report

Report Created: 8/31/2016
Time: 9:09am

Mode: Selected Shapes

Input Grid Factor: 1.000000

Original Surface: sCA0602_SOUTH_INTCHNG

Description: DTM_GROUND
Preference: Default
Type: Existing

Design Surface: Surface_Elevation_256_5

Description: Surface elevation of 256.5
Preference: Default
Type: Design

Cut Factor: 1.0000

Fill Factor: 1.0000

Cut: 304255.70 cu ft
Fill: 0.00 cu ft
Net: 304255.70 cu ft

Cut: 11268.73 cu yd
Fill: 0.00 cu yd
Net: 11268.73 cu yd

East Pond
Existing storage below elevation
256.5

Existing surface is set to Original
Surface and elevation 256.5 is set
to the Design Surface.
The Fill would indicate the amount
of fill below elevation 256.5.
The grading limits were used as a
boundary.

A fill of 0 shows no existing
storage in this area.

Triangle Volume Report

Report Created: 8/31/2016
Time: 9:16am

Mode: Selected Shapes

Input Grid Factor: 1.000000

Original Surface: sCA0602_SOUTH_INTCHNG

Description: DTM_GROUND
Preference: Default
Type: Existing

Design Surface: Surface_Elevation_256_5

Description: Surface elevation of 256.5
Preference: Default
Type: Design

Cut Factor: 1.0000

Fill Factor: 1.0000

Cut: 281177.57 cu ft
Fill: 98410.22 cu ft
Net: 182767.35 cu ft

Cut: 10413.98 cu yd
Fill: 3644.82 cu yd
Net: 6769.16 cu yd

West Pond
Existing storage below elevation
256.5

Existing surface is set to Original
Surface and elevation 256.5 is set
to the Design Surface.
The Fill would indicate the amount
of fill below elevation 256.5.
The grading limits were used as a
boundary.

98,410.22 cf / 43,560 sf/Ac-ft
**= 2.26 Ac-ft of existing storage in
this area**

Triangle Volume Report

Report Created: 8/6/2016
Time: 2:32pm

Mode: Selected Shapes

Input Grid Factor: 1.000000

Original Surface: Proposed_SouthCompArea_1

Description: South Comp Area Pond
Preference: Finished Surface
Type: Design

Design Surface: Surface_Elevation_256_5

Description: Surface elevation of 256.5
Preference: Default
Type: Design

Cut Factor: 1.0000

Fill Factor: 1.0000

Cut: 0.00 cu ft
Fill: 369878.40 cu ft
Net: -369878.40 cu ft

Cut: 0.00 cu yd
Fill: 13699.20 cu yd
Net: -13699.20 cu yd

South Comp Area
East Pond

Comparison of the new grading
against elevation 256.5.
Contour 256.5 was used as a
boundary.

Total storage from new grading
369,878.40 cf / 43,560 sf/Ac-ft
= 8.49 Ac-ft total storage

Triangle Volume Report

Report Created: 8/31/2016
Time: 8:56am

Mode: Selected Shapes

Input Grid Factor: 1.000000

Original Surface: Proposed_SouthCompArea2

Description:

Preference: Default

Type: Design

Design Surface: Surface_Elevation_256_5

Description: Surface elevation of 256.5

Preference: Default

Type: Design

Cut Factor: 1.0000

Fill Factor: 1.0000

Cut: 0.00 cu ft

Fill: 249455.66 cu ft

Net: -249455.66 cu ft

Cut: 0.00 cu yd

Fill: 9239.10 cu yd

Net: -9239.10 cu yd

South Comp Area
West Pond

Comparison of the new grading
against elevation 256.5
Contour 256.5 was used as a
boundary.

Total storage from new grading
249,455.66 cf / 43,560 sf/Ac-ft
= 5.73 Ac-ft total storage

Total storage available from new
grading
East Pond = 8.49 Ac-ft
West Pond = 5.73 Ac-ft
TOTAL = 14.22 Ac-ft

Need to calculate the existing
storage available below elevation
256.5 in both areas.

West Pond
See Triangle Volume Report for
InRoads Printout
2.26 Ac-ft of existing storage

East Pond
All new grading is below elevation
256.5. Therefore, all storage
available is new storage.
0 Ac-ft existing storage

NEW AVAILABLE STORAGE
14.22 Ac-ft from new grading
- 2.26 Ac-ft from existing storage

= 11.96 Ac-ft of new storage

8 Lane Option
3/15/2016

Surface to Surface Comparisons

Area	Fill from Existing to			Fill from 252 to Water Table	Proposed (A)	Fill Elev 248.6 to Proposed (E)	Fill Elev 249.6 to Proposed (F)	Fill Elev 252 to Proposed (B)	Proposed Fill Below 252* (D)	Ac-ft
	Elev 248.6	Elev 249.6	Elev 252							
8-1	2,470		9,595	7,125	0	0	0	0	0	
8-2	254		2,153	1,899	12,805	12,805	8,288	4,263	2.64	
8-3	4,927		17,265	12,338	93,720	91,360	76,994	11,799	7.31	
8-4	120		2,635	2,515	0	0	0	0	0.00	
8-5	5		167	17,260	0	0	0	0	0.00	
8-6	0		118	118	652	999	551	101	0.06	
8-7	0		761	761	5,303	4,501	2,588	2,715	1.68	
8-8		0	287	287	0		0	0	0.00	
8-9		26	188	162	0		25	0	0.00	
8-10		3,186	7,920	4,734	2,066		2,339	1,905	0.10	
8-11		5,407	13,958	8,551	627		1,088	98	0.33	
8-12		89	20,617	20,528	0		742	0	0.00	
8-13		0	52,856	52,856	0		0	0	0.00	
8-14		0	110	110	0		0	0	0.00	
8-15 A		11,980	24,807	12,827	767		829	161	0.38	
8-15 B		65	518	453	20		120	0	0.01	
8-15 C		88	716	628	273		453	62	0.08	
8-15 D		0	16	16	0		42	0	0.00	
8-16		6,475	14,369	7,894	7,302		7,988	5,605	1.05	
8-17		0	96	96	516		760	438	0.05	
8-18	0		438	438	117	616	84	438	0.27	
8-19	196		1,161	965	0		0	0	0.00	
8-20	7,503		27,918	20,415	19,021	17,119	8,949	2,569	1.59	
8-21	0		92	92	292	520	223	69	0.04	
8-22	2,964		6,807	3,843	10,826	9,493	6,458	1,404	0.87	
8-23	0		103	103	4,787	5,855	4,684	103	0.06	
8-24	0		1,462	1,462	322	633	285	37	0.02	
8-25	0		0	0	0	0	0	0	0.00	
Totals			207,133		159,416		117,373	26,712	16.56	

10 Lane Option

Area	Surface to Surface Comparisons							Proposed (D) Below 252*	Ac-ft
	Fill from Existing to			Fill from 252 to Water Table	Fill Elev 248.6 to Proposed (E)	Fill Elev 249.6 to Proposed (F)	Fill Elev 252 to Proposed (B)		
	Elev 248.6	Elev 249.6	Elev 252						
10-1	2,470		9,595	0	7,125	0	0	0	
10-2	254		2,153	10,350	1,899	11,691	8,288	1,808	1.12
10-3	4,927		17,265	91,790	12,338	88,330	75,860	11,003	6.82
10-4	120		2,635	314	2,515	448	193	1	0.00
10-5	5		167	0	162	0	0	0	0.00
10-6	0		95	966	95	1,194	871	95	0.06
10-7	0		761	5,303	761	6,491	4,542	761	0.47
10-8			287	0	287		0	0	0.00
10-9			188	5	162		25	1	0.00
10-10			7,920	2,235	7,920		2,011	224	0.14
10-11			5,758	5,703	3,485		4,854	1,835	0.99
10-12			20,617	344	20,528		742	132	0.08
10-13			52,856	0	52,856		0	0	0.00
10-14			110	0	110		0	0	0.00
10-15 A			24,807	36,085	12,827		28,748	20,804	2.05
10-15 B			518	20	453		136	0	0.01
10-15 C			716	389	628		490	189	0.07
10-15 D			16	0	16		19	0	0.00
10-16			14,369	9,371	14,104		10,462	7,929	0.73
10-17			96	707	96		1,086	611	0.06
10-18	0		233	989	233	2,781	789	233	0.14
10-19	196		1,161	0	965	0	0	0	0.00
10-20	4,697		12,773	24,205	8,076	22,853	12,374	7,134	4.42
10-21	0		92	493	92	590	459	34	0.02
10-22	2,964		6,807	7,142	3,843	6,143	3,922	256	0.16
10-23	0		103	5,908	103	6,976	5,805	103	0.06
10-24	0		1,462	322	1,462	633	285	37	0.02
10-25	0		0	0	0	0	0	0	0.00
Totals			183,560	202,641			146,900	28,117	17.43

Triangle Volume Report

Report Created: 9/12/2016
Time: 9:33am

Mode: Selected Shapes

Input Grid Factor: 1.000000

Original Surface: 1019_2022_247 Bottom

Description:

Preference: Finished Surface

Type: Design

Design Surface: Surface_Elevation_252

Description: Merged prop surface north of the river

Preference: Finished Surface

Type: Design

Cut Factor: 1.0000

Fill Factor: 1.0000

Cut: 0.01 cu ft

Fill: 472789.31 cu ft

Net: -472789.30 cu ft

Cut: 0.00 cu yd

Fill: 17510.72 cu yd

Net: -17510.71 cu yd

Southeast pond, non-detention
area.
Comparison of the pond
surface to an elevation of 252.
472,789.31 cf
10.85 Ac-ft

Triangle Volume Report

Report Created: 9/12/2016
Time: 9:46am

Mode: Selected Shapes

Input Grid Factor: 1.000000

Original Surface: Proposed_1021_247_SlopedBottom

Description:

Preference: Frame

Type: Design

Design Surface: Surface_Elevation_252

Description: Merged prop surface north of the river

Preference: Finished Surface

Type: Design

Cut Factor: 1.0000

Fill Factor: 1.0000

Cut: 0.00 cu ft

Fill: 159968.25 cu ft

Net: -159968.25 cu ft

Cut: 0.00 cu yd

Fill: 5924.75 cu yd

Net: -5924.75 cu yd

Middle Pond Detention Area
Comparison of the pond surface to
an elevation of 252
159,968 cf
3.67 Ac-ft

Triangle Volume Report

Report Created: 9/12/2016
Time: 9:50am

Mode: Selected Shapes

Input Grid Factor: 1.000000

Original Surface: Proposed_104_247_SlopedBottom

Description:

Preference: Default

Type: Design

Design Surface: Surface_Elevation_252

Description: Merged prop surface north of the river

Preference: Finished Surface

Type: Design

Cut Factor: 1.0000

Fill Factor: 1.0000

Cut: 0.00 cu ft

Fill: 503948.61 cu ft

Net: -503948.61 cu ft

Cut: 0.00 cu yd

Fill: 18664.76 cu yd

Net: -18664.76 cu yd

North Pond Detention Area
Comparison of the pond surface to
an elevation of 252
503,949 cf
11.57 Ac-ft

Attachment D: Meeting Notes

City of North Little Rock Floodplains Coordination Meeting/ October 11th

ATTENDEES: Chris Wilbourn, Mark Callahan, Adam Wierciak, Bryon Russell
COPY TO: Jennifer Halstead, Earl Mott
PREPARED BY: Bryon Russell
DATE: October 11, 2016 3:00 PM CST
PROJECT: CA0602

Objectives

Discuss floodplain impacts on Dark Hollow

Summary

The team reviewed the US Army Corps of Engineers HECRAS model for Dark Hollow, potential impacts of the project on floodplains associated with Dark Hollow, and the conceptual mitigation plan for Dark Hollow. Chris Wilbourn responded that the City of North Little Rock has no issues with the conceptual mitigation plan.

We discussed the storm sewer modeling effort underway for the system discharging to the Fairman Ditch. Adam Wierciak and Bryon Russell presented information on drainage area mapping west of I-30 in North Little Rock, obtained from recent field work. A 60-inch pipe outfall was discovered along North Poplar Street which appeared to discharge southwest toward the North Little Rock Boys and Girls Club ball field. Chris Wilbourn indicated this outfall likely connects to the Pike Avenue tunnel, which discharges to the Arkansas River through a pump station. Consequently, it was decided that the drainage area to the 60-inch pipe outfall could be deleted from the drainage area contributing to the I-30 frontage road storm sewer system.

Chris Wilbourn reported that flooding is common in the area of West 13th Street and North Magnolia Street, but he believes this is due to pipe clogging rather than capacity issues.

Chris Wilbourn asked if the project team was aware of a new residential development going in the northeast quadrant of the I-40/North Hills interchange. He believes this development may have floodplain impacts. The project team is only responsible for floodplain impacts related to the I-30 project.

Action Items

Provide the City with the US Army Corps of Engineers model for Dark Hollow.

City of Little Rock Floodplains Coordination Meeting/ January 11th

ATTENDEES: Keli Wylie, Nathan Charles, Vince Floriani, Mark Callahan, John Cantabery, Adam Wierciak, Bryon Russell

COPY TO: Jennifer Halstead, Earl Mott

PREPARED BY: Bryon Russell

DATE: January 11, 2017 10:00 am CST

PROJECT: CA0602

Objectives

Discuss floodplain impacts on Fourche Creek

Summary

As a follow-up to the November meeting, Adam Wierciak and Bryon Russell had reviewed the floodplain information that had been provided by the City of Little Rock. A review of the models verified that I-30 is located in the “bathtub” area of Fourche Creek. The bathtub area is not included in the hydraulic models. There is a gap in the hydraulic models between the Hwy 365 (Springer Boulevard) crossing and the University Avenue crossing. Consequently, Nathan Charles stated that no hydraulic modeling of the I-30 improvements will be required. The City of Little Rock will require a volumetric analysis of the floodplain impacts only.

The project team has developed conceptual plans for a temporary maintenance of traffic ramp between I-440 westbound and I-30 northbound, as well as for a new I-30 bridge over the Fourche Creek floodplain and the UPRR Railroad. The floodplain fill for the temporary ramp has been estimated at 11.2 Ac-ft. The amount of permanent additional fill due to the piers for the proposed bridge over the Fourche Creek floodplain is estimated at 0.1 Ac-ft. Two potential floodplain compensation areas in the I-30/I-530/I-440 interchange have been identified. These compensation areas are capable of providing 11.9 Ac-ft of compensating floodplain storage.

The amount of temporary and permanent floodplain fill needed to construct the project will be determined by the Design-Builder. The Design-Builder will be responsible for developing a floodplain compensation plan and securing approval of the plan from the City of Little Rock and Pulaski County. Should the Design-Builder elect to construct the project as shown in the concept plans, the City has indicated they will accept the plan.

Action Items

Provide the City with these meeting notes for review.

AHTD and City of North Little Rock Maintenance Coordination Meeting/ February 27, 2017

ATTENDEES: Mark Headley, Johnathon Mormon, Chris Wilbourn, Mark Callahan, John Cantabery, Bryon Russell

COPY TO: Ben Browning, Keli Wylie, Earl Mott

PREPARED BY: Bryon Russell

DATE: February 27, 2017 3:00 PM CST

PROJECT: CA0602

Objectives

The purpose of the meeting was to discuss maintenance responsibilities for the conceptual storm sewer serving the west I-30 frontage road and outfalling to the Fairman Ditch.

Summary

An overview of the conceptual storm sewer outfall to Fairman Ditch was provided. It was emphasized that this is only a concept, prepared for the purpose of ensuring that a solution could be found that complies with all project design criteria, and that the Design-Build team will have the flexibility to change the design, as long as they comply with the RFP criteria. The concept was developed after looking at many alternatives over several months.

The west frontage road storm sewer system serves a large offsite area of NLR and drains north to the Fairman Ditch. The system contains inlets accepting offsite runoff that are very low in relation to the 25 year tailwater of Fairman Ditch. In order to prevent surcharging of these inlets, the design concept involves a pond and pump system at the Fairman Ditch outfall.

AHTD suggested that, for ease of maintenance, pond slopes should be no steeper than 4:1 and the pond bottom should normally be dry. In order to accomplish this, the pond bottom should be graded toward a deeper wet well, which would then be pumped to the adjacent Fairman Ditch. The pond bottom should be seeded with water tolerant grasses. These criteria will be included in the RFP.

The pond and pump will be within AHTD right of way, but AHTD does not normally maintain pump stations, while the City of NLR maintains four. Due to their familiarity with pump stations, it was suggested that the City maintain the Fairman Ditch pond and pump station. Chris Wilbourn will discuss with the mayor. The City would want the pump to be float-activated, with diesel backup power available.

The design concept also involves diverting the portion of the west frontage road drainage area south of the Union Pacific Railroad that currently drains north to Fairman Ditch, south to the Arkansas River. Modifications to the existing pump station at Cypress Street, maintained by the City of NLR, will possibly be required, both because of impacts from the bridge construction, and because of the increase in flow. The RFP will contain language advising of the need for these modifications.

Action Items

Chris Wilbourn will discuss maintenance of the pond and pump station with the mayor of North Little Rock.